



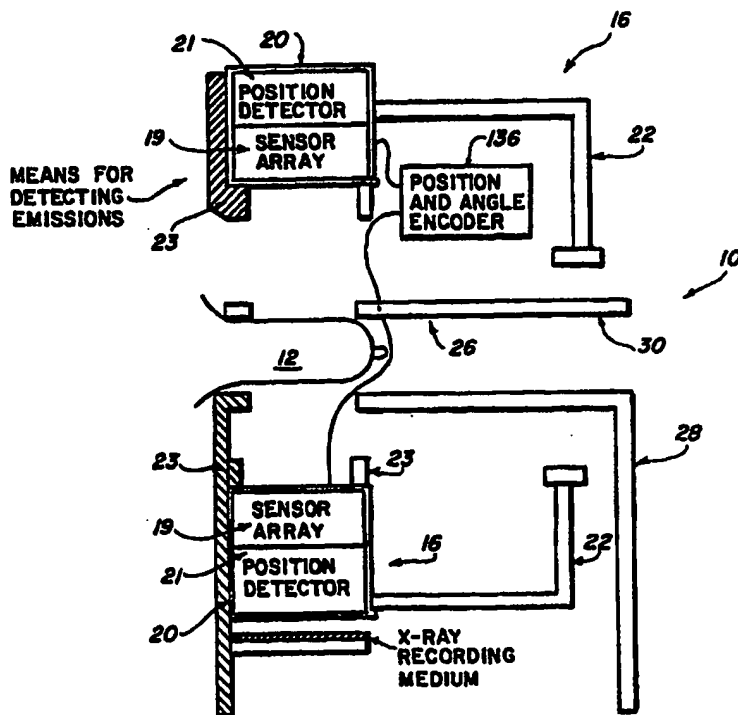
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(54) Title: DEDICATED APPARATUS AND METHOD FOR EMISSION MAMMOGRAPHY

(57) Abstract

The apparatus comprises a mechanism (x-ray recording medium) for providing an internal anatomical image of a body part (12) and a mechanism (19) for detecting single gamma-rays emitted by a radiotracer infiltrated into the body part.



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DEDICATED APPARATUS AND METHOD
FOR EMISSION MAMMOGRAPHY

CROSS REFERENCE

This is a continuation-in-part application of U.S.
5 serial number 08/063,450 filed May 18, 1993, now U.S. Patent
No. 5,323,006, issued June 21, 1994, which is a
continuation-in-part of U.S. serial number 07/824,804 filed
January 22, 1992, now U.S. Patent No. 5,252,830, issued
October 12, 1993.

10 FIELD OF THE INVENTION

The present invention is related to an apparatus
for medical examination. More specifically, the present
invention is related to an apparatus and method for imaging
the radiotracer concentration in a female breast or other
15 organ.

BACKGROUND OF THE INVENTION

Mammography is currently the most effective method
of screening for breast cancer. The goal of breast cancer
screening is the detection of early non-palpable tumors.
20 Although mammography is very sensitive in the detection of
cancer, it is not very specific in determining whether
mammographic abnormalities are due to benign or malignant
disease (Limitations of Mammography in the Identification of
Noninfiltrating Carcinoma of the Breast, S.F. Sener, F.C.
25 Candela, M.L. Paige, J.R. Bernstein, D.P. Winchester,
Surgery, Gynecology, and Obstetrics, Aug. 1988, 167:135-140).
Therefore, a noninvasive method of confirming the malignancy

-2-

of suspicious mammographic abnormalities would be a major benefit in patient care. In this way, the number of benign excisional biopsies (approximately 75% of all excisional biopsies) can be reduced.

5 When abnormal mammograms are encountered, the physician's options are limited. For minimally suspicious lesions, short-term repeat examination (four to six month follow-up) is often recommended. This may result in psychological stress for the patient and introduces the possibility of loss in patient follow-up due to scheduling or
10 communication errors. The unlikely possibility of interim tumor growth cannot be definitely ruled out (Breast Cancer: Age-Specific Growth Rates and Screening Strategies, M. Moskowitz, Radiology, Oct. 1986, 161:37-41), especially in
15 patients under fifty.

 The role of ultrasound in clarifying the status of a mammographic abnormality is limited to the differentiation of solid masses from benign cysts. If the strict criteria for the ultrasonic appearance of a simple cyst are satisfied,
20 the referring physician may be reassured that the lesion is benign. Unfortunately, the current spatial resolution of ultrasound makes the technique of limited value for lesions significantly smaller than five millimeters.

 Doppler ultrasound has been advocated as a means
25 for differentiating benign from malignant masses, but results of clinical trials have been contradictory, and the doppler method has no current clinical role in breast imaging (The Role of US in Breast Imaging, V.P. Jackson, Radiology, Nov. 1990, 177:305-311).

-3-

Fine-Needle Aspiration (FNA) of breast masses is a technique whose sensitivity and specificity is operator dependent (Fine-Needle Aspiration Biopsies of Breast Masses, L. Palombini et al., Cancer, June 1, 1988, 61:2273-2277), and
5 has been considered experimental (Discriminating Analysis Uncovers Breast Lesions, D.B. Kopans, Diagnostic Imaging, Sept. 1991, pp. 94-101). Because of its relatively low cost and reduced morbidity associated with surgery and anesthesia, FNA has been suggested as a possible replacement for
10 excisional biopsy. Unfortunately, there is a high (13-50%) rate of insufficient samples when FNA is performed on non-palpable mammographically detected lesions. All of these cases of negative FNAs require excisional biopsy (Fine-Needle Aspiration Cytology in Lieu of Open Biopsy in Management of
15 Primary Breast Cancer, H.J. Wanebo et al., Annals of Surgery, May 1984, 199 (5) pp. 569-579). Further, FNA as a non-imaging diagnostic modality, has the disadvantage that no information is obtained about the physical distribution of the detected tumor. As a cytopathological technique, FNA
20 cannot easily differentiate between cases of marked dysplasia, carcinoma-in-situ, or invasive cancer. Fine-Needle Aspiration is generally not performed for non-palpable breast lesions.

Another option for the referral of a patient with
25 equivocal mammographic anomalies is excisional biopsy of the breast in the area corresponding to the region of mammographic abnormality. The probability of malignancy ranges from 2% for a circumscribed solid mass to almost 90% for a spiculated ill-defined mass (Discriminating Analysis
30 Uncovers Breast Lesions, D.B. Kopans, Diagnostic Imaging, Sept. 1991, pp. 94-101. The true-positive fraction for biopsies obtained as a result of a mammographic screening

-4-

program is between twenty and thirty percent (Nonpalpable Breast Lesions: Accuracy of Prebiopsy Mammographic Diagnosis, G. Hermann, C. Janus, I.S. Schwartz, B. Krivisky, S. Bier, J.G. Rabinowitz, Radiology, Nov. 1987 165:323-326; 5 R. Brem, personal communication). Excisional biopsy has the additional disadvantage of introducing scarring, which may render interpretation of follow-up mammograms more difficult (Discriminating Analysis Uncovers Breast Lesions, D.B. Kopans, Diagnostic Imaging, Sept. 1991, pp. 94-101). An 10 additional disadvantage to excisional biopsies is that, as a non-imaging modality, the physical distribution of the tumor is poorly described.

It is also possible to use radionuclide imaging to detect cancers. 2-[F-18]-Fluoro-2-deoxy-D-glucose (FDG) is 15 a radioactive analogue of glucose that is taken up preferentially by cancer cells (Primary and Metastatic Breast Carcinoma: Initial Clinical Evaluation with PET with the Radiolabeled Glucose Analogue 2-[F-18]-Fluoro-2-deoxy-D-glucose, R.L. Wahl, R.L. Cody, G.D. 20 Hutchins, E.E. Mudgett, Radiology (1991) 179:765-770). A Fluorine-18 nucleus decays by emitting a positron which is annihilated within a millimeter by an electron. The result of this annihilation is the production of two 511 kev (thousand electron volts) gamma rays that are approximately 25 180 degrees apart in direction. After a patient has received an intravenous dose of FDG she may be examined with detectors that sense these gamma rays.

Previous detection methods have included imaging with a specially collimated planar gamma camera ([18-F] 30 Fluorodeoxyglucose scintigraphy in diagnosis and follow up of treatment in advanced breast cancer, European Journal of

-5-

Nuclear Medicine (1989) 15:61-66) and with a whole-body Positron Emission Tomography (PET) scanner (Primary and Metastatic Breast Carcinoma: Initial Clinical Evaluation with PET with the Radiolabeled Glucose Analogue 2-[F-18]-Fluoro-2-deoxy-D-glucose, R.L. Wahl, R.L. Cody, G.D. Hutchins, E.E. Mudgett, Radiology (1991) 179:765-770). PET imaging of breast cancer patients given FDG has been shown to be useful in imaging tumors as small as 3.2 cm and in patients whose breasts are too dense to be imaged well mammographically (Primary and Metastatic Breast Carcinoma: Initial Clinical Evaluation with PET with the Radiolabeled Glucose Analogue 2-[F-18]-Fluoro-2-deoxy-D-glucose, R.L. Wahl, R.L. Cody, G.D. Hutchins, E.E. Mudgett, Radiology (1991) 179:765-770).

15 The use of a specially collimated planar gamma camera to image the breast with this high resolution is limited by technical factors. The energy of 511 KeV is too penetrating to be detected well by conventional gamma cameras, and the collimation required to correct for the high
20 energy leads to loss of signal (counts/pixel) that is equivalent to resolution loss due to low photon flux.

Conventional PET imaging devices are designed to image cross sections of the entire body. Accordingly, there are several disadvantages to employing a whole body PET
25 scanner in a primary role as a high resolution confirmatory modality for small suspicious breast lesions. The first disadvantage of using a whole body PET scanner for breast imaging is the limited resolution available. The net resolution of a whole-body PET system is a combination of
30 individual factors and is limited to above 5 mm FWHM (E. Rota-Kops et al., Journal of Computer Assisted Tomography

-6-

- 1990, May-June 14 (3), pages 437-445; N.A. Mullani et al., Journal of Nuclear Medicine 1990, May 31 (5), pages 610-616 and pages 628-631; K. Wienhard et al., Journal of Computer Assisted Tomography 1992, Sept.-Oct. 16 (5) pages 804-813).
- 5 The effect of this resolution limit is that radioactivity is underestimated (Positron Emission Tomography and Autoradiography, Edited by M.E. Phelps, J.C. Mazziotta, H.R. Schelbert, pp. 240-285, Raven Press, N.Y. 1986; Design of a Mosaic BGO Detector System for Positron CT, H. Uchida, T.
- 10 Yamashita, M. Iida, S. Muramatsu, IEEE Transactions on Nuclear Science February 1986, NS-33 (1), pp. 464-467). This reduces the sensitivity of PET scanners in estimating the malignancy of mammographically detected lesions smaller than twice the resolution limit, and also precludes the use of the
- 15 PET scanner in delineating tumor margins with high accuracy.

A second disadvantage of a conventional PET scanner for imaging of subtle lesions in the breast is the high cost of the examination. In order to accommodate the entire body, a conventional PET scanner must employ tens or hundreds of

20 expensive detector arrays along with a gantry and associated electronics.

A third disadvantage of a PET scanner is that the PET image format would not be easily compared to conventional mammograms. This is due to the fact that the breast is an

25 organ which can be compressed to an essentially two-dimensional object. The variability in internal architecture of the breast results in few landmarks for positioning, and the location of an anomaly on the mammographic image of the compressed breast does not always

-7-

correspond to the same location in the non-compressed breast.

In order to achieve the highest spatial resolution available in a tomographic system, motion of the patient due to breathing must be limited. Immobilizing of the breast by
5 compression is the most straightforward approach to solving this problem, but implementation within a PET scanner detector ring is difficult. Additionally, the use of PET scanner to image an essentially two-dimensional object such as a compressed breast is not economically rational.

10 High resolution (20 cm diameter bore) PET scanners, originally developed for animal studies, may soon be available commercially. For a system with smaller aperture (i.e. 20 cm bore for a dedicated head scanner) the resolution in the axial plane is 3.5 mm (Development of a High
15 Resolution PET, T. Yamashita et al., IEEE Transactions on Nuclear Science, April 1990, Vol. 37 (2) pp. 594-599). Such a system would satisfy the goal of high resolution. A disadvantage would be the considerable cost of such relatively expensive scanners, with approximately fifteen
20 detector arrays, as dedicated units for breast imaging. Further, the problems of immobilization of the breast and of comparison to standard mammography would still be unaddressed.

SUMMARY OF THE INVENTION

25 The present invention is an apparatus for examining a body part. The apparatus comprises means or a mechanism for immobilizing and compressing the body part. The apparatus also comprises means or a mechanism for providing

-8-

an internal anatomical image of the body part and means or a mechanism for detecting single gamma-rays emitted by a radiotracer infiltrated into the body part. The detecting mechanism is disposed in an adjacent relationship with the
5 means or mechanism for providing an internal anatomic image so that the body part remains in the same position during and between anatomic and radiotracer imaging.

In one embodiment, the detecting means or mechanism includes a detector module disposed on one side of the
10 immobilizing means or mechanism. The detector module preferably has at least one array of gamma ray sensitive material in communication with a position detector. In another embodiment, the detecting means or mechanism includes a pair of detector modules disposed one on each side of the
15 immobilizing means or mechanism. Preferably, the means or mechanism for providing an anatomical image includes an x-ray source and x-ray recording medium.

The present invention is also an apparatus for examining a body part which comprises means or a mechanism
20 for immobilizing and compressing the body part and means or a mechanism for detecting single gamma-rays emitted by a radiotracer infiltrated into the body part.

The present invention is also an apparatus for examining a body part which comprises means or a mechanism
25 for immobilizing and compressing the body part and means or a mechanism for providing a stereotactic internal anatomical image of the body part. The apparatus also comprises means or a mechanism for providing a stereotactic physiological image of the body part in an adjacent relationship with the
30 means or mechanism for providing an internal anatomic image

-9-

such that the body part remains in the same position during and between stereotactic anatomic and radiotracer imaging.

Preferably, the means or mechanism for obtaining a stereotactic physiological image includes a pair of detector
5 modules disposed one on each side of the immobilizing means or mechanism. In one embodiment, the detector modules are constructed to travel angularly about the body part to provide projection images of the body part from at least two different viewing angles. In another embodiment, the
10 detector modules are stationary with respect to the body part and obtain multiple projection views of the body part.

The present invention is also an apparatus for examining a body part which comprises means or a mechanism for immobilizing and compressing the body part and means or
15 a mechanism for providing a stereotactic physiological image of the body part.

The present invention is also a method for examining a body part. The method comprises the steps of immobilizing the body part in a preferred position such that
20 the body part is compressed. Then there is the step of obtaining at least one physiological image of the body part. Preferably, before the immobilizing step, there is the step of injecting the patient with a radiotracer which emits gamma rays and the step of obtaining at least one physiological
25 image includes the step of detecting gamma-rays with at least one detector module disposed on at least one side of the body part. If desired, after the step of obtaining at least one physiological image, there can be the step of directing a biopsy needle or gun into the body part 12 using at least one
30 physiological image for guidance and placement. After the

-10-

step of obtaining the image or images, there can then be the step of operating on the patient using the image or images for guidance, localization, and preferably confirmation that the tumor has been removed completely. After the operating
5 step, there can be the step of obtaining at least one image of surgical specimens to identify the presence of and the borders of tumors.

BRIEF DESCRIPTION OF THE DRAWINGS

In the accompanying drawings, the preferred
10 embodiment of the invention and preferred methods of practicing the invention are illustrated in which:

Figure 1 is a schematic representation of an apparatus for examining a body part.

Figure 2 is a schematic representation showing a
15 close-up view of the detector modules of the apparatus for examining a body part.

Figures 3a and 3b are schematic representations showing the arrangement of the sensor array on the Photomultiplier (PMT).

20 Figure 4 is a schematic representation showing a plurality of imaging planes between the detector modules.

Figure 5 is a schematic representation of a gamma-ray stereotactic imaging apparatus with two gamma-ray detector modules configured for coincidence detection or for
25 dual-head single-emission acquisition.

-11-

Figure 6 is a schematic representation of a gamma-ray imaging apparatus with a gamma-ray detector module configured for single-head single-emission acquisition.

Figure 7 is a schematic representation of an x-ray stereotactic imaging apparatus.

Figure 8 is a schematic representation of a gamma-ray stereotactic imaging apparatus with mobile detector arrays.

Figure 9 is a schematic representation of a gamma-ray stereotactic imaging apparatus with stationary detector arrays.

DESCRIPTION OF THE PREFERRED EMBODIMENT

Referring now to the drawings wherein like reference numerals refer to similar or identical parts throughout the several views, and more specifically to figure 1 thereof, there is shown an apparatus 10 for examining a body part 12, such as a breast. The apparatus 10 includes means or a mechanism 14 for providing an anatomical image of the body part 12 and means or mechanism 16 for providing a physiological image of the body part 12. The means or mechanism 16 for providing a physiological image is disposed adjacent to the means or mechanism 14 for providing an anatomical image such that the body part 12 remains in the same position during and between anatomical and physiological imaging. Preferably, the body part 12 is infiltrated with a radiotracer and the means or mechanism 16 for providing a physiological image includes means or a mechanism for detecting emissions of the radiotracers from the body part

-12-

1 2 . The radiotracers can be
2-[F-18]-fluoro-2-deoxy-D-glucose (FDG) or 16
alpha-[F-18]-fluoroestradiol-17 beta or other radiotracers.
Preferably, the means or mechanism for providing an
5 anatomical image includes an x-ray source and x-ray recording
medium, such as x-ray film. Alternatively, a digital
radiography device can be used. Alternatively, other methods
of anatomic imaging such as magnetic resonance can be used.
Alternatively, other methods of anatomic imaging such as
10 ultrasound can be used.

In a preferred embodiment, the radiotracer produces
gamma rays and the detecting means or mechanism includes two
detector modules 20 each of which has at least one sensor
array 19 of gamma ray sensitive material (scintillator), such
15 as bismuth germanate (BGO) crystals, mounted upon a position
detector 21 such as a photomultiplier array or position
sensitive photomultiplier. Alternatively, individual light
sensors, such as avalanche photodiodes can be mounted upon
each gamma ray detector in the array 19. In an alternative
20 embodiment, each detector module 20 has a continuous sheet of
gamma ray detecting material which is mounted upon a position
sensitive multiplier or photomultiplier array. The
continuous sheet of gamma ray sensitive material can have
slots with septa on its surface which would operate in a
25 manner similar to the block detectors known in the art of PET
scanners.

Preferably, each detector module 20 has dense
shielding 23 for reducing undesirable emissions from other
parts of the body. Preferably, each detector module 20 is
30 attached to a swing arm 22 for allowing them to swing into
and out of an operational portion. Preferably, the apparatus

-13-

10 includes means or a mechanism 26 for immobilizing the body part 12, such as with compression. The immobilizing means or mechanism 26 can include a table 28 and a compression arm 30 which compresses the body part 12 against the table 28.

5 In an alternative embodiment, the apparatus 10 is not limited to having means or a mechanism 14 for obtaining an anatomical image of the body part 12. The apparatus 10 includes means or mechanism 26 for immobilizing the body part 12 and means or mechanism 16 for providing a physiological
10 image of the body part 12. The providing means or mechanism 16 is in an adjacent relationship to the immobilizing means or mechanism 26. Preferably, the immobilizing means or mechanism 26 compresses the body part 12 and can include a table 28 upon which the body part 12 rests and a compression
15 arm 30 which compresses the body part against the table 28. Alternatively, the apparatus could include an immobilizing means or mechanism 26 consisting of a C-arm for intra-operative tumor localization.

The invention is also a method of examining a body
20 part of a patient. The method includes the first step of immobilizing the body part in a preferred position. Then, there is the step of obtaining a physiological image of the body part. Preferably, before the immobilizing step, there is the step of injecting the patient with a radiotracer and
25 the obtaining step includes the step of detecting emissions from the immobilized body part. The step of obtaining an anatomical image of the body part such as an x-ray can be performed before the immobilizing step. Preferably, before the immobilizing step, there is the step of performing a
30 compression examination, such as a spot view compression examination.

-14-

The invention is also related to an alternative method of examining a body part of a patient. This method includes the first step of obtaining an anatomical image of the body part. Then, there is the step of obtaining a physiological image of the body part such that the body part remains in the same position during and between anatomical and physiological imaging. Preferably, before the obtaining step, there is the step of immobilizing the body part, such as with compression.

10 In the operation of the apparatus 10, a patient who is being examined for breast cancer would be injected with 2-[F-18]-Fluoro-2-deoxy-D-glucose (FDG). FDG is a radiotracer which is a radioactive analogue of glucose that is taken up preferentially by breast cancer cells. A more
15 detailed explanation of this process is given in Primary and Metastatic Breast Carcinoma: Initial Clinical Evaluation with PET with the Radiolabeled Glucose Analogue 2-[F-18]-Fluoro-2-deoxy-D-glucose, R.L. Wahl, R.L. Cody, G.D. Hutchins, E.E. Mudgett, Radiology (1991) 179:765-770,
20 incorporated by reference. The isotope 18-F decays by emitting a positron which is annihilated within a few millimeters by an electron. The result of this annihilation is the production of two gamma rays that are approximately 180° apart in direction.

25 Approximately one hour after injection with FDG, the patient undergoes a spot view breast compression examination. The breast 12 would then be immobilized and a mammogram would be obtained for any areas suspicious for malignancy. If an abnormality is spotted on the mammographic
30 film, high resolution detector modules 20 are swung in place above and below the compressed breast. Each detector module 20 consists of an array of bismuth germanate crystals which

-15-

detect the gamma rays produced by the FDG. Each array is mounted upon a position sensitive photomultiplier. Electronic collimation using coincidence gating would yield high sensitivity to emitted radiation. The shielding reduces the number of undesirable emissions detected by the detector modules. Once the detector modules are swung into place an image of the emissions is taken in areas of suspicion.

The rationale for the apparatus is the adaptation of the standard radiological mammographic geometry for the detection of gamma rays produced by positron-emitting and gamma-emitting radiotracers. The apparatus would incorporate (or be easily mounted upon) a conventional or x-ray mammography unit for straightforward comparison with conventional mammograms.

The increased sensitivity allowed by the mammographic geometry is expected to permit imaging of suspicious areas in the breast within a short period of time (10-15 minutes), allowing the patient to remain in breast compression for the duration of the scan. Use of the invention results in exact registration between the conventional mammogram and the image of radiotracer uptake. Advantages of the invention over existing technology include high resolution, low cost, reduced dose, and decreased morbidity.

The proximity of the detector modules to the breast in the proposed mammographic geometry will lead to resolution superior even to high resolution PET scanners. Since image reconstruction via filtered backprojection is not required in this geometry, no loss of resolution due to frequency filtering will be encountered.

-16-

The dose of radioactivity given to the patient will be similar to or less than the dose presently used for whole body PET imaging of FDG (approximately ten millicuries), which is within the acceptable radiation dose for diagnostic
5 nuclear medicine techniques. The morbidity associated with this dose must be compared to the morbidity associated with unnecessary excisional biopsy. For treatment planning, the morbidity may be compared to that associated with unnecessary mastectomy. For delineation of tumor margin, the morbidity
10 should be compared to the local recurrence of tumor in an under-resected breast.

Positron emitters such as Fluorine-18 (half-life 110 minutes) can be purchased by breast imaging centers from cyclotrons in most major U.S. cities. Note that the use of
15 the proposed dedicated breast imaging device does not preclude the possibility of following the examination with a whole body PET scanner (if available) when clinically indicated, i.e., to search for metastases in a patient with proven cancer. Additionally, by placing a collimator upon
20 one or both of the detector modules, and operating the apparatus in a non-coincident mode, the apparatus could be used in conjunction with more generally available radioisotopes that emit single photons. Additionally, the apparatus could be taken to the operating room for
25 intra-operative tumor localization.

If a radiotracer is used whose decay results in the production of opposing gamma rays, such as 2-[F-18]-Fluoro-2-deoxy-D-glucose, the present invention envisions an apparatus 100 which is capable of 3-dimensional
30 imaging and offers optimal spatial resolution and sensitivity. As shown in figure 2, the apparatus 100 is

-17-

comprised of a first detector module 120 for detecting radiotracer emissions from the body part 12 and a second detector module 121 for detecting radiotracer emissions from the body part 12. The first and second detector modules 120, 5 121 are disposed adjacent to each other with the body part 12 disposed therebetween. The apparatus 100 also comprises means or a mechanism 102 for backprojecting detected coincident events with respect to the first and second detector modules 120, 121 onto a plurality of imaging planes 10 132 between the first and second detecting modules 120, 121. The imaging planes 132 are shown in figure 4.

Preferably, the first detector module 120 is comprised of a first sensor array 122 of material sensitive to emissions from the radiotracer and the second detector 15 module 121 is comprised of a second sensor array 123 of material sensitive to emissions from the radiotracer.

Preferably, as illustrated in figure 4, the backprojecting means or mechanism 102 comprises means or a mechanism for defining a line 130 between a point on the 20 first sensor array 122 and a point on the second sensor array 123 associated with a coincident event and means or a mechanism for determining the intersection of the line 130 with each imaging plane 132. Preferably, the apparatus 100 also comprises means or a mechanism for determining the 25 distance, d , and angle, a , between the first detector module 120 and the second detector module 121, such as a position and angle encoder 136. Preferably, each of the first and second detector modules 120, 121 comprises a position detector, such as imaging PMT (photo multiplier) 108. 30 Preferably, the apparatus 100 also comprises means or a mechanism 104 for displaying the imaging planes such as a

-18-

digital gamma camera display and acquisition system. Preferably, each of the sensor arrays 122, 123 are comprised of a large array of BGO crystals (20x20 to 40x40).

The present invention is also a method of examining
5 a body part 12. The method comprises the step of detecting a plurality of coincident events associated with the interaction of radiotracer emissions from the body part 12 with a first and second sensor array 122 and 123. Then, there is the step of backprojecting the detected coincident
10 events onto a plurality of imaging planes 132 between the first and second sensor arrays 122 and 123.

Preferably, the backprojecting step includes the step of defining a line 130 between a point of the first sensor array 122 and a second point of the second sensor
15 array 123 associated with the coincident event and determining the intersection of the line 130 with each imaging plane 132. Preferably, after the backprojecting step, there is the step of displaying the plurality of imaging planes.

20 In the operation of the apparatus 100, the patient is injected with 2-[F-18]-flouro-2-deoxy-D-glucose (FDG). As shown in figures 3a and 3b, each of the detector modules 120, 121 comprises a Hamamatsu R394I-02 Imaging PMT 108 with an array 122, 123 of 37 x 37 BGO crystals above and below a
25 breast 12. The width of each array 122, 123 is 75 mm, as represented by reference character A. Each crystal is 2 x 2 x 7 mm. The top of each crystal is cut at the optimal angle 25° to break the symmetry to maximize the light collected by the PMT 108. The exact length (7 mm above) is
30 a compromise between efficiency and resolution. One wishes

-19-

to maximize the efficiency (make the crystals longer) while minimizing the multiple interactions which will blur the image (make the crystals shorter) ("Single Interaction PET Detectors" C.A. Burnham, J.T. Elliot, D.E. Kaufman, D.A. Chesler, J.A. Correia, and G.L. Brownell. Conference Record of the 1990 IEEE Nuclear Science Symposium PP: 1332-1336 1990, incorporated by reference.

This sensor array design is based on the belief that techniques which would measure the number of interactions are too complicated to be practical ("Resolution and Sensitivity Improvement in Positron Emission Tomography by the First Interaction Determination" Z.H. Cho and S.C. Juh. IEEE 1991 Medical Imaging Conference (Santa Fe) Record pp. 1623-1627). The effect of multiple interactions is reduced, by reducing the probability of their occurrence. This thin sensor array design will have reduced efficiency, but the other detection possibilities gained by allowing all crystals to be in coincidence will more than make up for this. Oblique rays would normally require the measurement of the depth of interaction in each crystal to maintain good spatial resolution ("A PET Detector with Depth-of-Interaction Determination" P. Bartzakos and C.J. Thompson. Phys. Med. Biol. V 36, pp. 735-748 (1991), but these crystals will be short enough to make this measurement unnecessary. Alternatively, a crystal block cut from the top and bottom with the bottom cuts offset from the top cuts by half the cut separation could be used to reduce the parallax error caused by oblique incidence on a deep detector.

The first and second detectors modules 120, 121 are separable by raising the upper one. The distance, d , between them would be variable in order to accommodate anatomical

-20-

variations. The angle, a , between them would be variable to accommodate imaging of organs such as the prostate, that might require non-parallel arrangement of the detector modules.

5 Each imaging PMT 108 would be connected to three analog-to-digital converters (ADCs) to measure the X and Y coordinates and the observed energy of the gamma ray produced by the FDG radiotracer. The PMTs 108 would be connected to a coincidence circuit and the backprojecting means or
10 mechanism 102 in order to detect the gamma rays produced by positron annihilations in the region between them. In principle coincidences between any crystal in the first and second sensor arrays 122, 123 will be permitted. It is from the diagonal coincidences, and the current detector module
15 separation, d , and angle, a , that the depth of the event can be determined.

When an annihilation occurs between the first and second sensor arrays 122, 123 the 511 keV gamma pair may travel in such directions that they will interact with the
20 first and second arrays 122, 123. As one ray enters a crystal it has a 20 to 30% chance of interacting with it, depending on the crystal depth and the photon direction. Of these events, 45% are photo-electric, depositing 511 keV in one crystal only. The shape of the crystals is such that
25 most of the light photons created in such events are detected by the PMT 108, making good energy identification possible (Probably better than 10% full-width at half-maximum [FWHM] energy resolution). The Compton scattered rays from the other 55% of the interactions will be scattered onto a cone
30 whose most probable apex angle is 45° and will deposit 50 keV in the crystal at a depth of 3 mm. The 461 keV ray will then

-21-

escape and interact beyond the crystal. For this reason the electronics for event detection should be sensitive to the 511 keV photons from photo-electric events and 25-150 keV photons corresponding to single Compton interactions of 511 keV photons, and should be able to discriminate against the single Compton interactions on the basis of their lower energy.

If two such photons (one in each detector module) are detected within the resolving time, a coincidence has occurred, and a line corresponding to the most probable depth of interaction in the two crystals is calculated. This is done by using the effective detector separation, d , (see figure 2) and the coordinates of the crystals of the first and second sensor arrays 122, 123 which interacted with the coincident rays.

With reference to figure 4, the coordinates of the crystal in the first sensor array 122 is X_U, Y_U and the coordinates of the crystal in the second sensor array 123 is X_L, Y_L . The event is thus localized on the line 130:

$$\begin{aligned} X_i &= X_L + a_i (X_U - X_L) \\ Y_i &= Y_L + a_i (Y_U - Y_L) \\ a_i &= Z_i/d \dots \dots \dots (i=1 \text{ to } n) \end{aligned} \quad (1)$$

It is not possible to determine the parameter a_i , which would locate the point of annihilation uniquely in 3-dimensional space. However, by assuming a value for a_i and thus defining an imaging plane 132, the X_i and Y_i coordinates could be determined for that imaging plane 132. Supposing the detectors modules 120, 121 are 6 cm apart, 13 values for a_i ranging from -3.0 cm to +3.0 cm are chosen. From equation

-22-

1, one can calculate 13 pairs (X_i, Y_i) of coordinates which correspond to the intersections of the line 130 given by equation 1 and the imaging planes 132 defined by $Z = -3.0$ to $Z = 3.0$ in 5 mm intervals. These sets of coordinates can now
5 be considered as points in a 128 by 128 by 16 matrix. All 16 of these matrix elements are augmented. [One does not know where the event really occurred, but by assigning the event (augmenting a memory location) at each level all possibilities are provided for]. Augmenting a memory
10 location means or mechanism to add a small positive number to it. The magnitude of this number depends on the relative crystal pair efficiency, and the attenuation path length.

After placing the breast section to be examined between the two detectors modules 120, 121, the first or
15 upper detector module 120 is lowered into place. The detector module separation, d , is measured with a position encoder 136. The position encoder 136 is read to calculate an angle scaling factor. Position determining look up tables are then calculated and saved in the data acquisition
20 system's processor's tables which are part of the backprojecting means or mechanism 102. Acquisition takes place for a preset time, some 30-50 minutes after the IV FDG injection. When a coincidence is detected, the intersection points with possible 13 imaging planes are calculated by
25 looking in the tables. The resulting 13 coordinates are presented to a modified gamma camera interface, which is set up to do a gated study. The 13 coordinate pairs are presented in turn, as if they were in separate phases of the cardiac cycle. Thus, all imaging planes 132 are augmented,
30 via a read-modify-write memory cycle. Preferably, the point of intersection of the line and each imaging plane is proportional to the photon attenuation along that line

-23-

divided by the product of the crystals' relative sensitivities.

At the end of the study, the data can be displayed on display means or mechanism 104 with conventional gamma camera display software. Note there is no reconstruction, as the memories contain the normalized projection data ready for display. Each imaging plane 132 contains an image of all data acquired throughout the study. The data has been, in effect "back-projected" onto all 13 imaging planes, by adding the same number to different locations in each imaging plane 132.

An analogy can be made with conventional X-ray tomography in which an X-ray tube and film move in an elliptical motion above and below the patient. The image is formed as an "in focus" image of the plane through which a line joining the focal spot and one point on the film passes through the same point in the patient. Attenuation from other points is blurred by the relative motion. In the present invention, each imaging plane 132 contains data from annihilations which truly occurred near that plane, and all others. As in the case of the X-ray tomography, the data which truly originated in that plane is in focus, that from other planes is blurred.

The 13 imaging planes 132 can now be examined one by one, or all can be displayed at once. The lower display threshold is raised until the background in normal tissue is almost "black". At this point, "hot spots" will appear in regions of high glucose metabolism, and "cold spots" in regions of low glucose metabolism. For either cold or hot spots, the section which contains the highest contrast, or

-24-

best defined boundaries, is the one which localizes the abnormality best. Conventional Gamma Camera software for smoothing, contouring, measurement of area, and enhancement can be used to process and interpret the image.

- 5 Assuming that the same breast compression was used for a conventional mammogram, the conventional and emission mammographic images can be registered precisely.

10 To calibrate the apparatus 100, a plastic box having the dimensions of the largest compressed breast section likely to be imaged, is filled with FDG solution. The normal scanning technique is used and the table used to augment memory locations is filled with the value $Ke^{\mu p}$ (where μ is the linear attenuation coefficient for 511 keV gamma rays in water, 0.098 cm^{-1} and p is the geometrical path length. The crystal efficiency tables in memory are all set to "1". Data is then acquired for about one hour.

20 At the end of the calibration scan all memory locations would have the same number of counts if all path lengths were equal, and all detector modules 120, 121 were equally efficient. They will have different numbers however due to counting statistics, and different crystal pair efficiencies. These will show up as variations in the calibration images. The line of response joining each crystal pair is then forward projected through all slices, and this is divided into the average value for all crystal pairs in order to derive the crystal efficiency table.

25 This calibration technique combines inter-crystal sensitivity and attenuation correction into the backprojection operation scaling, making possible real time

-25-

image formation. The only difference is that rather than adding "1" to each memory location, a number which compensates for attenuation and inter-crystal sensitivity is added. Assuming the memory depth is only 16 bits, this
5 number must be scaled to prevent quantization errors and overflows. It is anticipated that a number of the order of 100 would be used, with a range of 70 to 130. It may also be necessary to introduce a distortion correction as well in case the imaging response of the PMTs is nonlinear.

10 The apparatus 100 can be coupled to a minimally modified Gamma Camera acquisition and display computer capable of gated studies. All the calibration tables and line of response (LOR) calculations are self contained, but the highly developed Nuclear Medicine image processing
15 software is well suited for use with the apparatus 100.

The fact that no image reconstruction is required, but spatial localization in all three axes is possible by backprojecting scaled values along each LOR, mimicking a gated study. This simple technique provides a simple imaging
20 system with the best possible spatial resolution, and real time display of the images during formation. A similar approach to spatial localization has been discussed for applications unrelated to breast imaging (Performance Parameters of a Positron Imaging Camera, by G. Muehlenner,
25 M.P. Buchin, and J.H. Dudek, IEEE Transactions on Nuclear Science, Vol. NS-23, No. 1, February 1976).

The present invention also envisions use of dedicated instrumentation for emission mammography in conjunction with radiotracers that emit single gamma rays
30 and/or photons. Figure 5 shows a gamma-ray stereotactic

-26-

imaging apparatus with two gamma-ray detector modules configured for coincidence detection or for dual-head single-emission acquisition. Radiotracers that decay by positron emission result in the production of a pair of gamma rays. Although such radiotracers are known to be highly accurate in the detection of breast cancer, recent reports in the literature have supported a role for single photon, gamma ray emitters such as Technetium-99m (A. Waxman et al., Journal of Nuclear Medicine, Vol. 34, Issue 5, Page 139P). Advantages to using such emitters include low cost and ease of availability as compared to positron emitters.

The apparatus 10 as described above would be adaptable for application to single photon emitters by using one or both of the detector modules 20 to detect activity from the compressed breast. (See figures 5 and 6.)

Coincidence circuitry would not be required for single emission systems. Note that reports are present in the literature (Lee et al., Journal of Nuclear Medicine, Vol. 34, Issue 12, Pages 2095-2099, and A. Waxman et al., Journal of Nuclear Medicine, Vol. 34, Issue 5, Page 139P, incorporated by reference herein) describe the use of gamma cameras to detect activity from the breast from single photon and positron emitters. The difference between these reports and the present invention is that the present invention incorporates breast immobilization and/or compression during acquisition of data. Several advantages are realized as a result of this feature, which are enumerated as follows:

1. Since the breast contains few landmarks, internal details such as tumors will not be reproducibly localized unless immobilization/compression is used.

-27-

Reproducible localization is essential if the emission image is to be used for interventions such as biopsy or placement of localizing needles for surgeons.

2. Immobilization/compression allows confident
5 registration to be performed with x-ray images, thereby increasing diagnostic confidence in the ability of the emission image to characterize a lesion initially detected by x-rays.

3. Compression reduces the volume of tissue being
10 imaged with the gamma-ray detectors to the region of clinical interest. This reduction in volume of tissue results in decreased attenuation of the gamma ray beam on its way from the lesion to the gamma-ray detector. Decreased attenuation will lead to increased count density, which is advantageous
15 since the image is of higher diagnostic quality and since the dose to the patient can be reduced.

As shown in figure 7, stereotactic guidance is a technique employed by radiologists to direct biopsies using x-ray images. The technique consists of the acquisition of
20 two projection images that differ in projection angle. The data afforded by having the two images allows the depth of a lesion to be assessed, just as the human brain can assess the depth of an object by integrating information from both eyes. As applied to mammography, the lack of internal stable
25 structures in the breast require that the breast be immobilized during acquisition of both projections, without releasing compression between acquisitions. Several manufacturers (Fischer Corporation and Lorad Corporation) have designed mammography units in which software and display
30 interfaces allow the stereotactic images to be inspected by

-28-

a physician, and when a lesion is identified on both views a computer calculates the expected depth of the lesion. When the coordinates of the lesion are generated by the computer, the physician can enter the coordinates into a biopsy gun
5 mount so that biopsies of the lesion can be reliably obtained.

As is known in the art, biopsy guns incorporate hollow needle assemblies that allow a core of tissue to be removed. Surgeons often request that hooks, needles, or dyes
10 be placed in a suspicious lesion under mammographic guidance so that the surgeon can later identify the lesion in the operating room. Placement of such localizing hardware can be accomplished using stereotactic guidance.

One application of the present invention to use
15 stereotactic guidance to provide projection images that can be used for stereotactic biopsy guidance. In a stereotactic x-ray mammographic unit (figure 7), the x-ray detector module travels a certain angle between the stereotactic views (usually 15 degrees) while the patient's breast 12 is under
20 compression. In the present invention, as shown in figure 8, the gamma-ray detector modules 20 can be positioned so as to travel a specified angle as well.

Alternatively, since the gamma cameras obtain information from many projections, it is possible to have the
25 gamma ray detector modules 20 remain in a single location while multiple projection views were obtained for stereotactic guidance (figure 9). The projections obtained from such projection views can be inspected by a human operator to detect a lesion. If the lesion is visible on
30 more than one projection view, calculations similar to those

-29-

performed for x-ray stereotactic guidance can be performed to determine the depth of the lesion. The coordinates of the lesion can then be used to guide biopsy.

Heretofore, stereotactic guidance has never been
5 done using gamma cameras. The principal advantage of
stereotactic guidance using gamma ray imaging relates to the
requirement for sampling or excising lesions which might be
only detectable using gamma-ray imaging techniques. It is a
medical dictum that a detection method is not helpful if the
10 results cannot be confirmed by biopsy, and current gamma
cameras and positron emission tomography scanners are not
well-suited to guide biopsies. This is due to the large size
of these imaging devices and their relatively poor detection
efficiencies which necessitate long acquisitions times. The
15 requirement that a patient remain in compression for
acquisition of the stereotactic views and for biopsy implies
that high quality images be obtained in short times. The
present invention allows this to happen because the detectors
are so close to the breast, and because compression reduces
20 the amount of attenuating tissue between the lesion and the
detectors.

Note that the stereotactic capability of the
invention allows biopsy guidance to be performed on the basis
of the emission images alone or in conjunction with the x-ray
25 images, since the gamma-ray detectors are in the same
geometry as the conventional x-ray detectors. Thus an area
of suspicion by x-ray criteria could be localized by x-ray
stereotactic guidance and the presence or extent of the
lesion confirmed by gamma-ray imaging prior to biopsy.
30 Alternatively, if no lesions were identifiable by x-ray
criteria, and the emission images identified a suspicious

-30-

lesion, the biopsy could be guided on the basis of the emission images alone.

The present invention is an apparatus 10 for examining a body part 12. The apparatus comprises means or a mechanism 26 for immobilizing and compressing the body part and means or a mechanism 14 for providing an internal anatomical image of the body part. The apparatus also comprises means or a mechanism for detecting single gamma-rays emitted by a radiotracer infiltrated into the body party in an adjacent relationship with said means or mechanism for providing an internal anatomic image such that the body part 12 remains in the same position during and between anatomic and radiotracer imaging.

In one embodiment, as shown in figure 6, the detecting means or mechanism includes a detector module 20 disposed on one side of the immobilizing means or mechanism 26. The detector module 20 preferably has at least one array of gamma ray sensitive material in communication with a position detector. In another embodiment, as shown in figure 5, the detecting means or mechanism includes a pair of detector modules 20 disposed one on each side of the immobilizing means or mechanism 26. Preferably, each detector module has at least one array of gamma-ray sensitive material in communication with a position detector. Preferably, the means or mechanism 14 for providing an anatomical image includes an x-ray source and x-ray recording medium.

The present invention is also an apparatus for examining a body part which comprises means or a mechanism 26 for immobilizing and compressing the body part and means or

-31-

a mechanism for detecting single gamma-rays emitted by a radiotracer infiltrated into the body part 12. The detecting means or mechanism can include a detector module disposed on one side of the immobilizing means or mechanism or on both
5 sides. If desired, there can be included means or a mechanism for providing an internal anatomical image of the body part, such as an x-ray device.

The present invention is also an apparatus for examining a body part 12 which comprises means or a mechanism
10 26 for immobilizing and compressing the body part 12 and means or a mechanism 100 for providing a stereotactic internal anatomical image of the body part (figure 7). The apparatus also comprises means or a mechanism 102 for providing a stereotactic physiological image of the body part
15 in an adjacent relationship with the means or mechanism 100 for providing an internal anatomic image such that the body part remains in the same position during and between anatomic and radiotracer imaging.

Preferably, the means or mechanism 102 for
20 obtaining a stereotactic physiological image includes a pair of detector modules 20 disposed one on each side of the immobilizing means or mechanism 26. In one embodiment, as shown in figure 8, the detector modules 20 are constructed to travel angularly about the body part 12 to provide projection
25 images of the body part 12 from at least two different viewing angles, as is well known with x-ray stereotactic imaging. In another embodiment, the detector modules 20 are stationary with respect to the body part 12 and obtain multiple projection views of the body part 12.

-32-

The present invention is also an apparatus for examining a body part 12 which comprises means or a mechanism 26 for immobilizing and compressing the body part and means or a mechanism 102 for providing a stereotactic physiological
5 image of the body part. As stated previously, detector modules 20 can be positioned to travel angularly about the body part 12 to provide projection images of the body part from at least two different viewing angles or detector modules can be stationary with respect to the body part 12
10 and multiple projection views of the body part are obtained to form a stereotactic image.

The present invention is also a method for examining a body part 12. The method comprises the steps of immobilizing the body part 12 in a preferred position such
15 that the body part 12 is compressed and obtaining a stereotactic physiological image of the body part. Preferably, before the immobilizing step, there is the step of injecting the patient with a radiotracer which emits gamma rays and the step of obtaining a stereotactic physiological
20 image includes the step of detecting gamma-rays with a pair of detector modules 20 disposed one on each side of immobilizing means or mechanism. Preferably, before the step of obtaining a stereotactic physiological image, there is the step of obtaining a stereotactic internal anatomical image of
25 the body part 12. If desired, after the step of obtaining a stereotactic physiological image, there can be the step of directing a biopsy needle or gun into the body part 12 using the stereotactic physiological image for guidance and placement.

30 Moreover, after the step of obtaining an image, for example, a single image or stereotactic images, there can be

-33-

the step of operating on the patient using the obtained radiotracer image or images for guidance and localization.

The present invention is also a method for examining a body part 12. The method comprises the steps of
5 immobilizing the body part 12 in a preferred position such that the body part 12 is compressed and obtaining at least one physiological image of the body part. Preferably, before the immobilizing step, there is the step of injecting the patient with a radiotracer which emits gamma rays and the
10 step of obtaining at least one physiological image includes the step of detecting gamma-rays with at least one detector module 20 on at least one side of the immobilizing means or mechanism. If desired, after the step of obtaining at least one physiological image, there can be the step of directing
15 a biopsy needle or gun into the body part 12 using at least one physiological image for guidance and placement. After the step of obtaining the image or images, there can then be the step of operating on the patient using the image or images for guidance, localization, and preferably
20 confirmation that the tumor has been removed completely. After the operating step, there can be the step of obtaining at least one image of surgical specimens to identify the presence of and the borders of tumors.

Herein, means or mechanism for language has been
25 used. The presence of means is pursuant to 35 U.S.C. §112 and is subject thereto. The presence of mechanism is outside of 35 U.S.C. §112 and is not subject thereto.

Although the invention has been described in detail in the foregoing embodiments for the purpose of illustration,
30 it is to be understood that such detail is solely for that

-34-

purpose and that variations can be made therein by those skilled in the art without departing from the spirit and scope of the invention except as it may be described by the following claims.

-35-

WHAT IS CLAIMED IS:

1. An apparatus for examining a body part comprising:

means or a mechanism for immobilizing and compressing the body part;

means or a mechanism for providing an internal anatomical image of the body part; and

means or a mechanism for detecting single gamma-rays emitted by a radiotracer infiltrated into the body part in an adjacent relationship with said means or mechanism for providing an internal anatomic image such that the body part remains in the same position during and between anatomic and radiotracer imaging.

2. An apparatus as described in Claim 1 wherein the detecting means or mechanism includes a detector module disposed on one side of the immobilizing means or mechanism, said detector module having at least one array of gamma ray sensitive material in communication with a position detector.

3. An apparatus as described in Claim 1 wherein the detecting means or mechanism includes a pair of detector modules disposed one on each side of the immobilizing means or mechanism, each detector module having at least one array of gamma-ray sensitive material in communication with a position detector.

-36-

4. An apparatus as described in Claim 1 wherein the means or mechanism for providing an anatomical image includes an x-ray source and x-ray recording medium.

5. An apparatus for examining a body part comprising:

means or a mechanism for immobilizing and compressing the body part; and

means or a mechanism for detecting single gamma-rays emitted by a radiotracer infiltrated into the body part.

6. An apparatus as described in Claim 5 wherein the detecting means or mechanism includes a detector module disposed on one side of the immobilizing means or mechanism, said detector module having at least one array of gamma ray sensitive material in communication with a position detector.

7. An apparatus as described in Claim 5 wherein the detecting means or mechanism includes a pair of detector modules disposed one on each side of the immobilizing means or mechanism, each detector module having at least one array of gamma-ray sensitive material in communication with a position detector.

8. An apparatus as described in Claim 5 including means or a mechanism for providing an internal anatomical image of the body part.

9. An apparatus for examining a body part comprising:

-37-

means or a mechanism for immobilizing and compressing the body part;

means or a mechanism for providing a stereotactic internal anatomical image of the body part; and

means or a mechanism for providing a stereotactic physiological image of the body part in an adjacent relationship with said means or mechanism for providing an internal anatomic image such that the body part remains in the same position during and between anatomic and radiotracer imaging.

10. An apparatus as described in Claim 9 wherein the means or mechanism for obtaining a stereotactic physiological image includes a pair of detector modules disposed one on each side of the immobilizing means or mechanism.

11. An apparatus as described in Claim 10 wherein the detector modules can be positioned to travel angularly about the body part to provide projection images of the body part from at least two different viewing angles.

12. An apparatus as described in Claim 10 wherein detector modules are stationary with respect to the body part and obtain multiple projection views of the body part.

13. An apparatus for examining a body part comprising:

means or a mechanism for immobilizing and compressing the body part; and

-38-

means or a mechanism for providing a stereotactic physiological image of the body part.

14. An apparatus as described in Claim 13 wherein the means or mechanism for obtaining a stereotactic physiological image includes a pair of detector modules disposed one on each side of the immobilizing means or mechanism.

15. An apparatus as described in Claim 13 wherein the detector modules can be positioned to travel angularly about the body part to provide projection images of the body part from at least two different viewing angles.

16. An apparatus as described in Claim 13 wherein detector modules are stationary with respect to the body part and obtain multiple projection views of the body part to form a stereotactic image.

17. A method for examining a body part comprising the steps of:

immobilizing the body part in a preferred position such that the body part is compressed; and

obtaining at least one physiological image of the body part.

18. A method as described in Claim 17 wherein the obtaining step includes the step of obtaining a stereotactic physiological image of the body part.

-39-

19. A method as described in Claim 18 wherein before the immobilizing step, there is the step of injecting the patient with a radiotracer which emits gamma rays and the step of obtaining a stereotactic physiological image includes the step of detecting gamma-rays with a pair of detector modules disposed one on each side of immobilizing means or mechanism.

20. A method as described in Claim 19 wherein before the step of obtaining a stereotactic physiological image, there is the step of obtaining a stereotactic internal anatomical image of the body part.

21. A method as described in Claim 17 wherein after the step of obtaining a stereotactic physiological image, there is the step of directing a biopsy needle or gun into the body part using the stereotactic physiological image for three-dimensional guidance.

22. A method as described in Claim 21 wherein after the step of obtaining a stereotactic image, there is the step of operating on the patient using the obtained stereotactic image for guidance and localization.

23. A method as described in Claim 17 including after the step of obtaining the image, there is the step of operating on the patient using the image for guidance, localization, and confirmation that any tumor of the body part has been removed completely.

24. A method as described in Claim 23 including after the operating step, there can be the step of obtaining

-40-

at least one image of surgical specimens to identify the presence of and the borders of tumors.

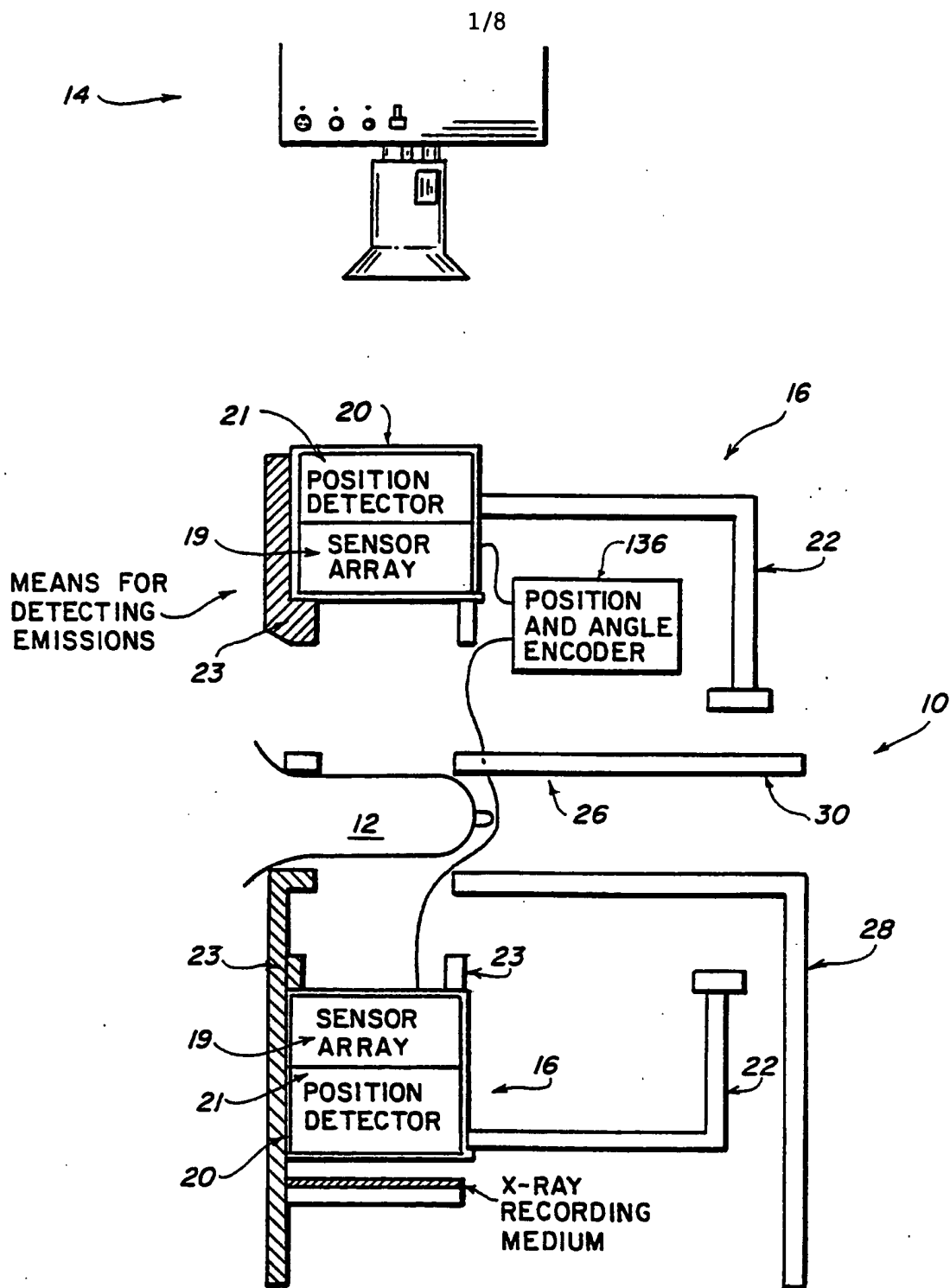
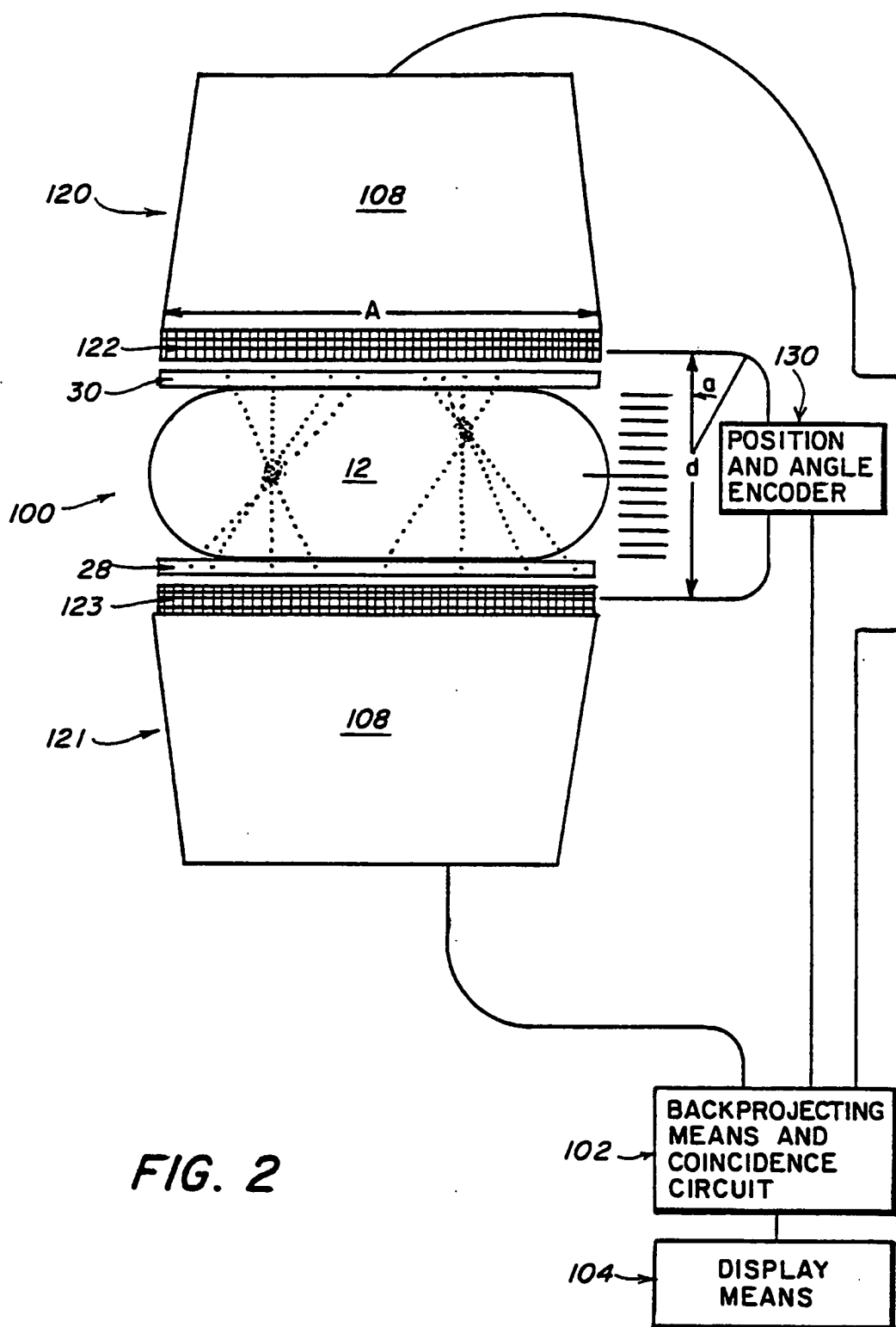


FIG. 1

2/8



3/8

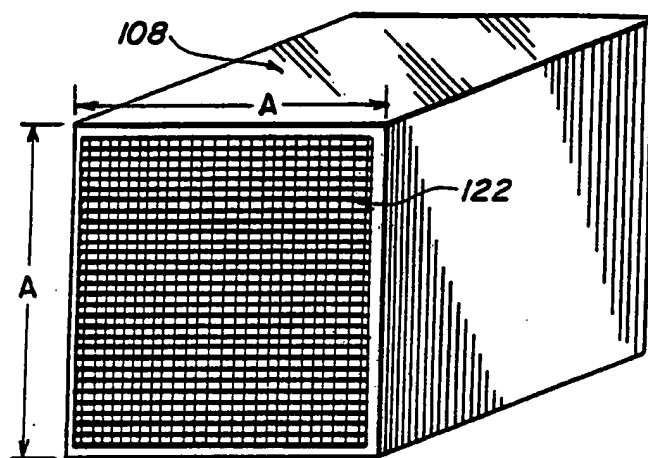


FIG. 3a

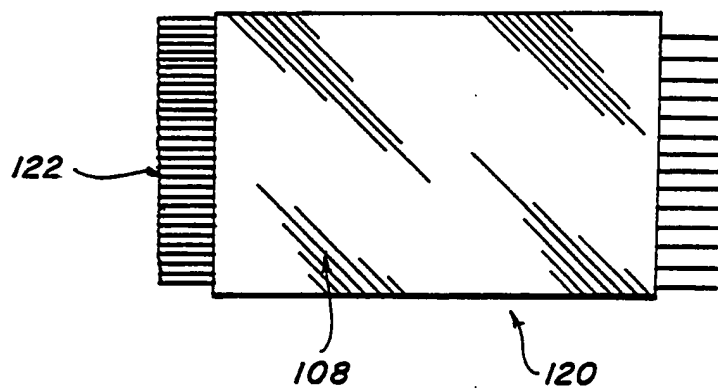
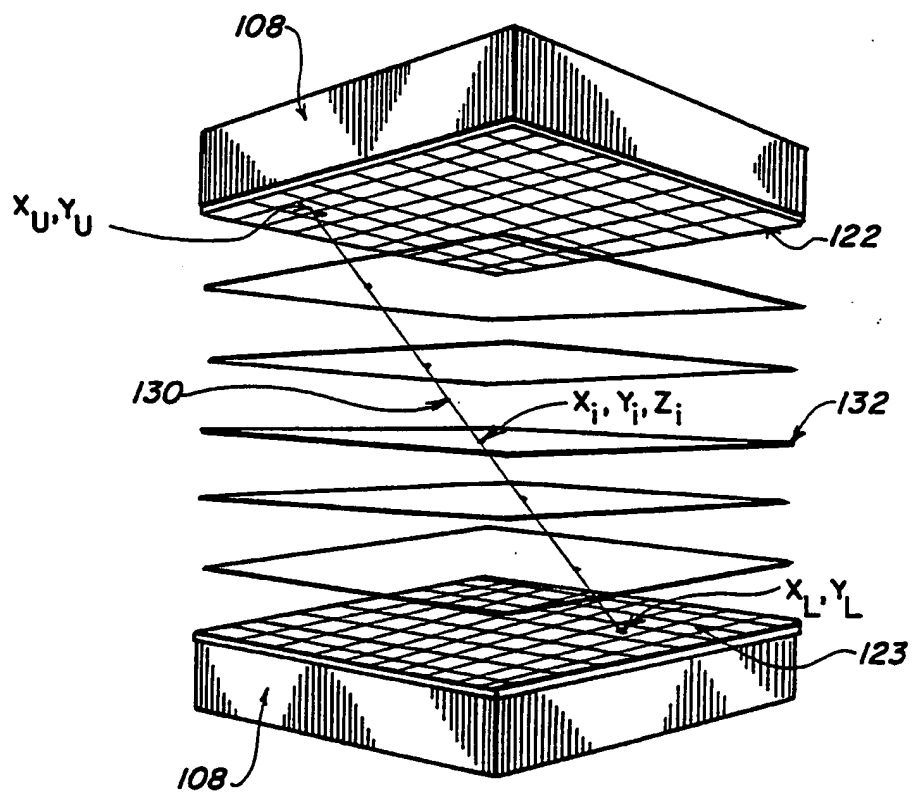
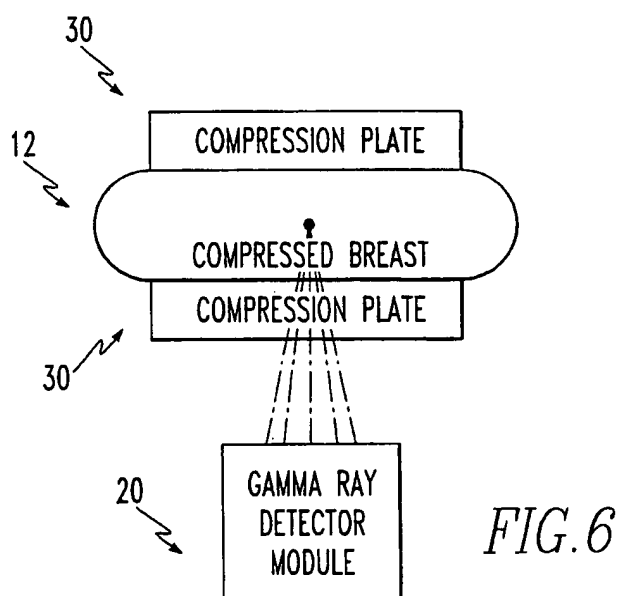
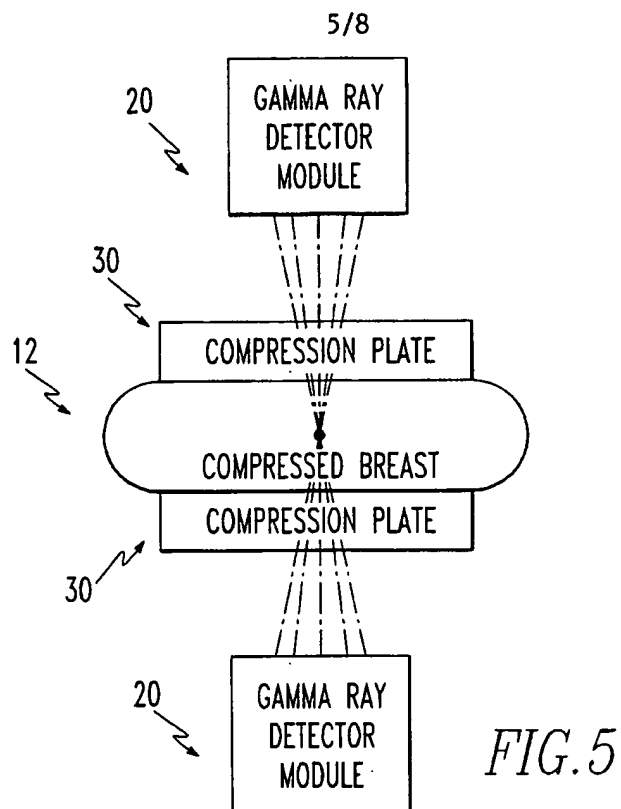


FIG. 3b

4/8

**FIG. 4**



6/8

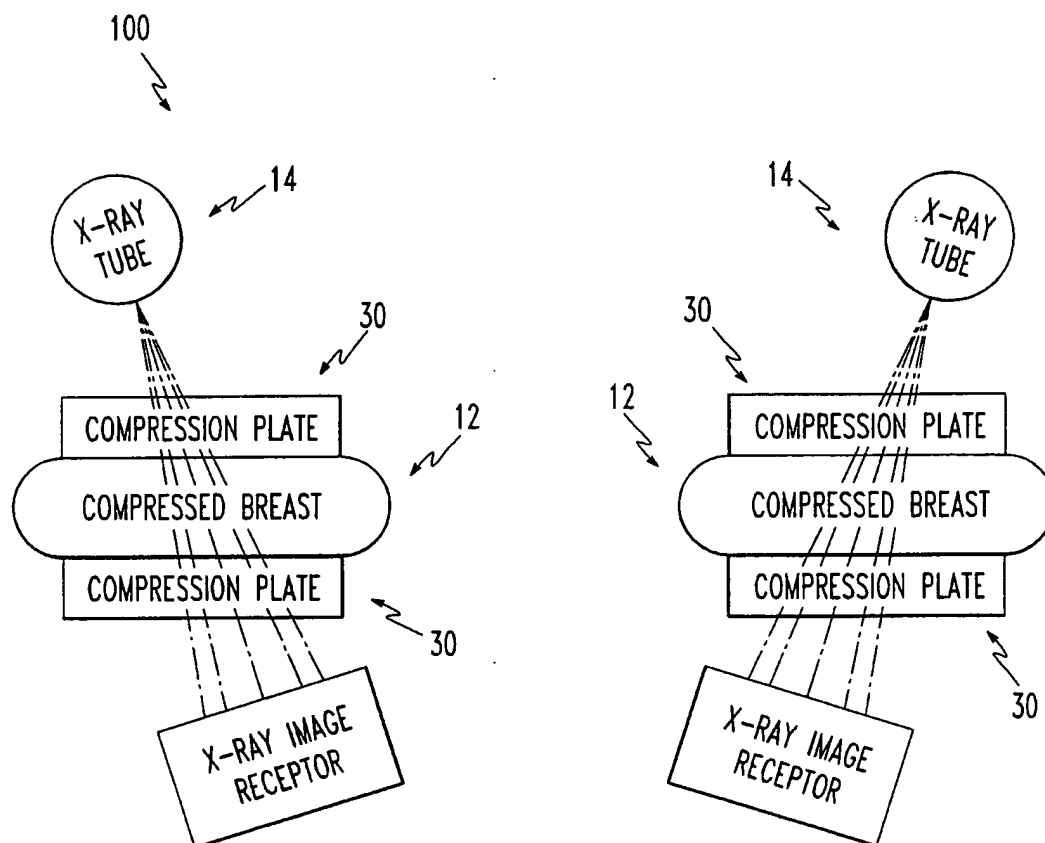


FIG. 7

7/8

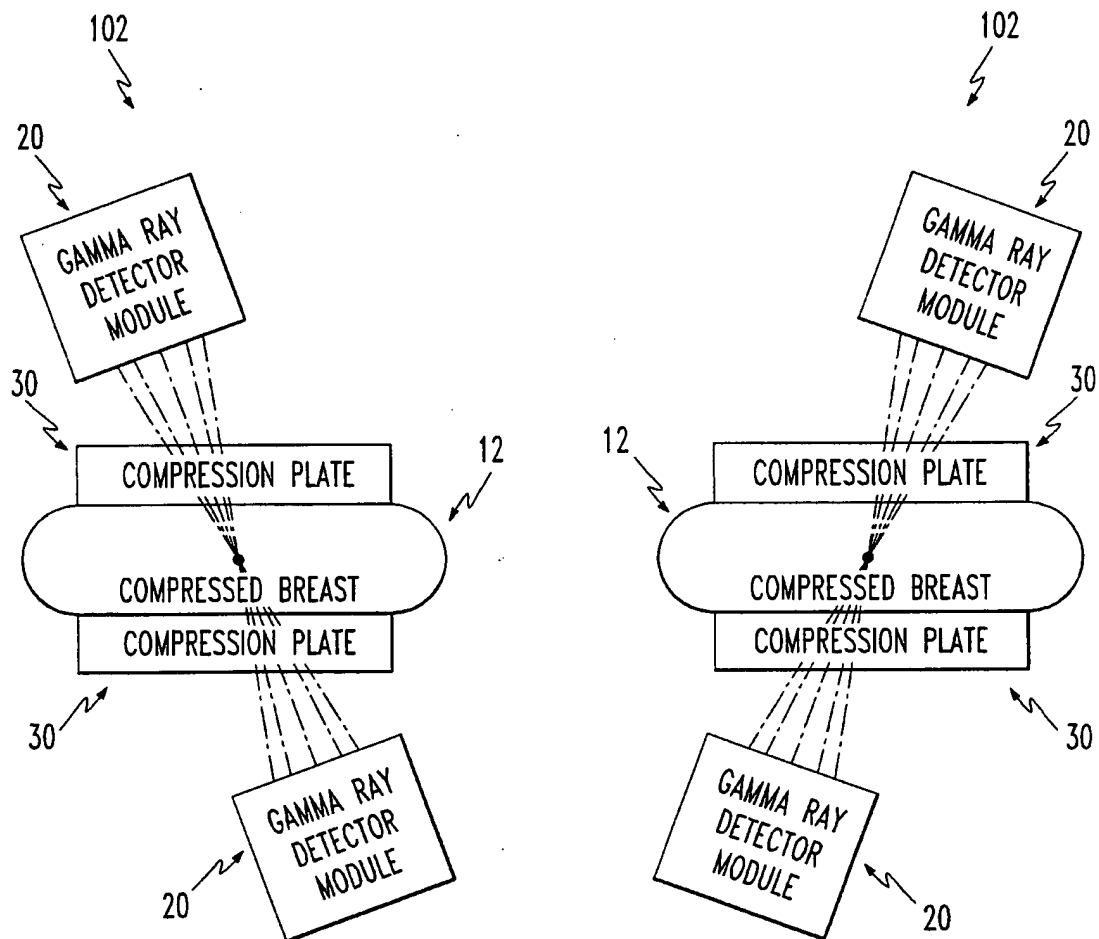


FIG. 8

8/8

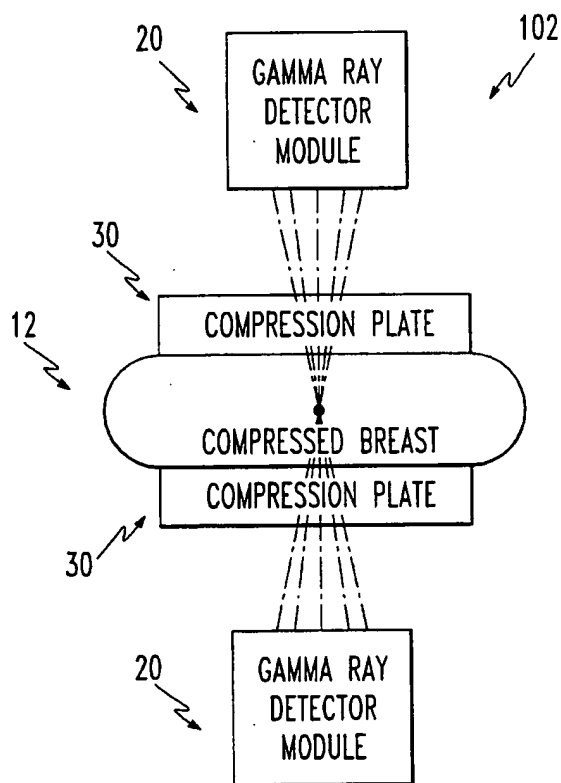


FIG. 9

INTERNATIONAL SEARCH REPORT

international application No.
PCT/US95/08397

A. CLASSIFICATION OF SUBJECT MATTER

IPC(6) :G01T 1/161
US CL :250/363.02; 378/37

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

U.S. : 250/363.02, 363.04; 378/37

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

APS

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	US, A, 5,252,830 (Weinberg) 12 OCTOBER 1993 entire document.	1-4
Y	US, A, 5,051,257 (Pietronigro) 24 September 1991, entire document.	5-24
Y	JP, A, 59-180477 (Hatsutori) 13 October 1984, entire document.	5-24
Y	WO 93/17620, A, (Siczek) 16 Sep 1993, entire document.	5-24

☐ Further documents are listed in the continuation of Box C. ☐ See patent family annex.

* Special categories of cited documents:	*T later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
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Date of the actual completion of the international search

01 SEPTEMBER 1995

Date of mailing of the international search report

07 SEP 1995

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